

# Feasibility of Saline Gradient Solar Ponds as Thermal Energy Sources in Saskatchewan, Canada

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**ABSTRACT.** Advancement of renewable energy is critical for sustainable development. This paper evaluates the feasibility of saline gradient solar ponds (SGSP) as an alternative energy source for Saskatchewan, Canada. The main achievements include global appraisal of SGSP from theoretical and practical perspectives, assessment of salinity and climatic criteria for SGSP potential, understanding of heat transfer mechanisms affected by thermophysical properties, and numerical modeling to simulate transient heat diffusion in SGSP. Results indicated that Saskatchewan is ideal for thermal energy harvesting from saline water bodies because of high solar insolation (1100 to 1400 kWh/m<sup>2</sup>). The solar radiation in such systems is captured under a salt concentration gradient. Locally, ten potash tailings sites (360 g/L or 36% salt) and two saline water lakes (250 g/L or 25% salt) are potentially suitable for SGSP deployment. It was found that thermal conductivity increases with temperature but decreases with water salinity increase (0.55 to 0.675 W/mK) and the opposite is true for density (1000 to 1200 kg/m<sup>3</sup>). Similarly, specific heat capacity slightly increases with temperature and inversely correlates with salinity (3000 to 4200 J/kg K). Furthermore, the heat diffusion model adequately simulated the temperature distribution for a typical SGSP in a potash tailings containment facility. For the investigated month of July (highest solar insolation), the temperatures increased from an initial value of at 20 to 52 °C at top to 37 °C at bottom. A comprehensive risk assessment of this method is required to protect air, water, soil, and biota at specific sites.

**Keywords:** salinegradient solar ponds, thermal energy, natural lakes, tailings ponds, heat diffusion

## 1. Introduction

The ever-growing demand for energy means that an increased amount of hydrocarbon fuels (such as oil, gas, and coal) will continue to be used in the foreseeable future (International Energy Agency, 2014) because of their abundance and ease of use. This is especially true for low-grade heat generation that is associated with a temperature increase of up to 50 °C above ambient conditions (Wang and Ma, 2015). To effectively mitigate the adverse effects of hydrocarbon combustion on the atmosphere (such as CO<sub>2</sub> emissions and green-house effects), there is an enhanced interest in exploring alternative energy options. Although high energy outputs can be achieved through photovoltaic solar panels and wind or water turbines (Jacobson and Delucchi, 2011), high capital and operational costs and intermittent availability are the main limitations of most of the emerging methods.

A saline gradient solar pond (SGSP) can provide an energy solution that is environmentally friendly (because of negligible emissions), cost effective (offering low initial and maintenance

expenses), and socially acceptable (already operative in natural lakes). Such a system requires a shallow water body with appropriate quantities of dissolved salts and an adequate amount of solar radiation prevalent at the site. This thermal phenomenon was first reported in Lake Madoc (Romania) with bottom temperatures of up to 70 °C at 1.3 m depth (Kalecsinsky, 1902). Likewise, the mechanism has been shown to work under cold conditions such as Lake Vanda (Antarctica) that is covered with 3 ~ 4 m thick ice layer and exhibits 25 °C temperature at its deepest parts (Abdullah et al., 2017).

SGSP has been adapted in man-made systems such as tailings containment facilities (that is, ponds containing post-extraction waste slurries) with appropriate chemical composition. Successful applications of SGSP have been reported for mineral production (Lesino and Saravia, 1991; Garrido et al., 2012; Montalà et al., 2019) and desalination processes (Lu et al., 2001; Garman and Muntasser, 2008; Saleh et al., 2011). More importantly, SGSP is applicable to potash solution mining for providing heat energy for on-site utilization. For example, Aimone-Martin and Martell (2000) developed such a system for mineral crystallization at a facility in New Mexico, USA (cold semi-arid climate) where a low relative humidity and an adequate cloud cover contribute to a high annual solar insolation of up to 1900 kWh/m<sup>2</sup>. Saskatchewan (Canada) is quite suitable for the deployment of this technology because it has

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natural saline lakes and potash tailings ponds with adequate salt concentrations (25 ~ 360 g/L) and it receives an annual solar insolation between 1100 to 1400 kWh/m<sup>2</sup> (Ito and Azam, 2018).

The main objective of this study was to evaluate the feasibility of SGSPs as a thermal energy sources in the area. First, the typical mechanism of SGSP is presented and the practical experience with this technology from around the globe is summarized. Second, the mean daily global insolation for 415 municipalities was retrieved from the Photovoltaic Potential and Insolation Database (Natural Resources Canada, 2018) and converted to monthly and annual values to develop a temporal correlation. Third, a spatial relationship was developed using the Google Earth web application to obtain the global positions of the municipalities and the saline water bodies. Fourth, potential SGSP sites were identified for possible implementation of this method. Fifth, the effect of thermophysical properties on the heat transfer mechanism was established to identify appropriate methods and limits operative in such systems. Finally, a conceptual heat diffusion model was developed for a potash tailings containment facility as a typical candidate for SGSP in Saskatchewan.

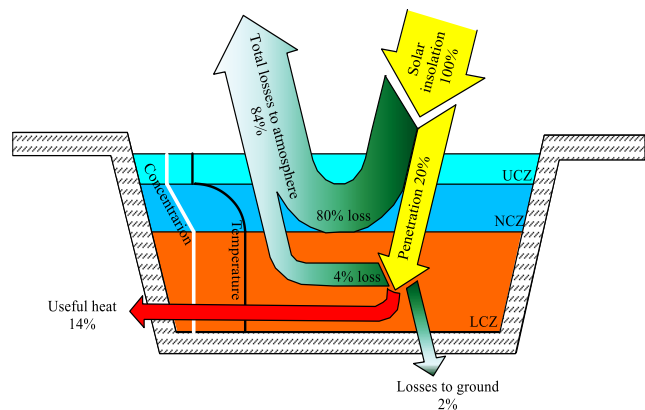
## 2. Literature Review

### 2.1. Theoretical Background

SGSP facilities collect solar energy in the form of heat that can be used for industrial processes, electricity generation, and space heating (French et al., 1985; Akbarzadeh et al., 2005). Figure 1 shows the conceptual model for SGSP in terms of energy balance and profiles of salt concentration and temperature (Ormat Turbines Ltd., 1981; Busquets et al., 2012; Ito and Azam, 2018). Solar radiation is captured under the salt concentration profile (Halocline) when the following three zones are established within the water body: (i) upper convective zone (UCZ), water layer with insignificant salinity and ambient air temperature; (ii) non-convective zone (NCZ), water layer with gradually increasing salinity (0% to 25% by mass) and temperature; and (iii) lower convective zone (LCZ), brine layer ( $\geq 25\%$  by mass) at higher temperatures.

Solar energy, entering into SGSP, is partially absorbed and transformed to thermal energy at the pond bottom. During this process, heat transfer in the NCZ (increasing salinity) is primarily governed by the diffusion phenomena through the Soret effect, that is, mass transfer of salt particles in the saline liquid results in heat transfer (Kim, 2013). Random Brownian motion at the molecular level takes place due to collisions under the thermal gradient to propagate heat in all directions (Guerrero et al., 2013). In contrast, the heat transfer mechanism in the UCZ (negligible constant salinity) and LCS (high constant salinity) is governed by diffusion and internal convection involving bulk fluid circulation due to temporal temperature fluctuations at the boundaries. Despite thermal effect, the fluid density difference imposed by the salt concentration difference largely suppresses global convection within the NCZ. Likewise, a stable salt concentration gradient allows solar radiation to reach to the LCZ and store heat even in the absence of sunlight (Gonzalez et al.,

2016).



**Figure 1.** Schematic of saline gradient solar pond with estimated energy balance and profiles of salt concentration and temperature (After Ormat Turbines Ltd., 1981; Busquets et al., 2012; Ito and Azam, 2018)

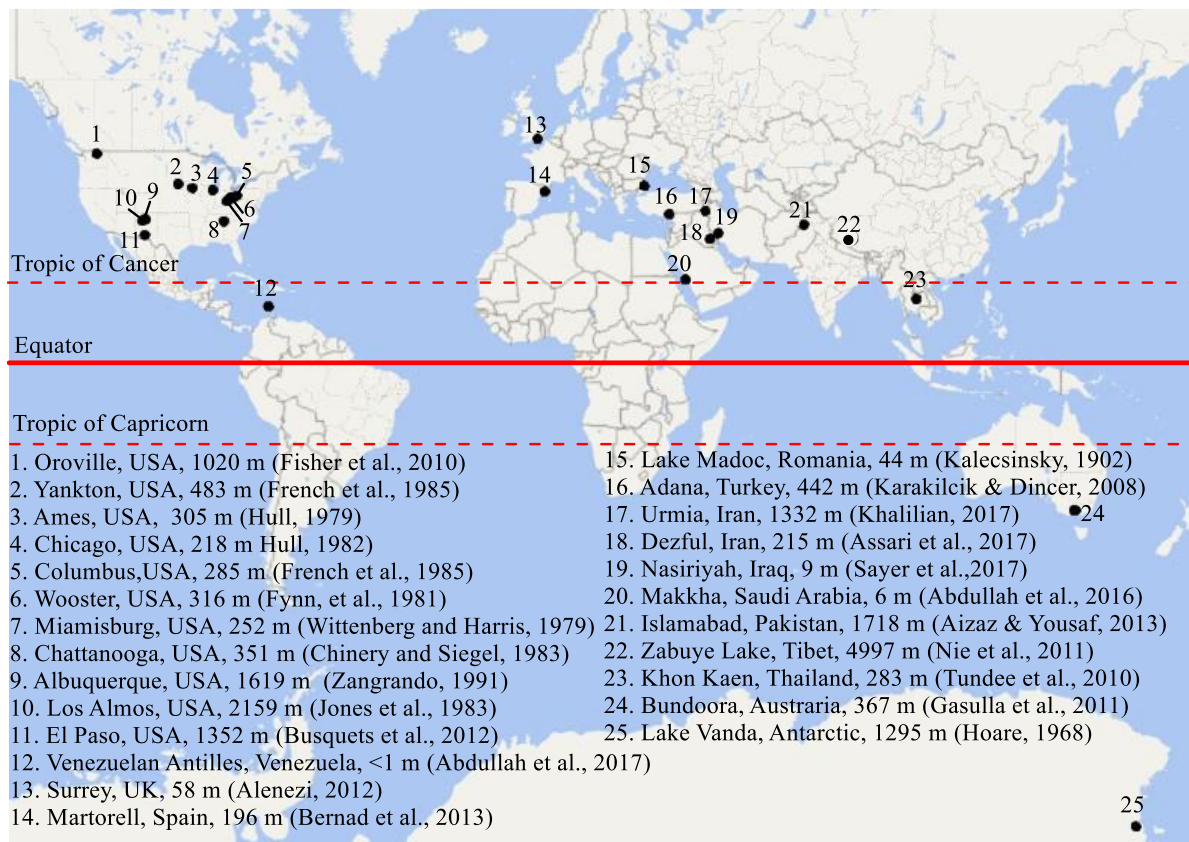
### 2.2. Practical Logistics

Heat is generally extracted from the lower layers through one of the two mechanisms. The SGSP at El Paso (USA) utilizes an external heat exchanger system that requires pumping of brine from the top of the LCZ at steady velocity along with a returning brine flow post heat extraction (Lu et al., 2004). In contrast, the SGSP at Pyramid Hill (Australia) uses an in-pond heat exchanger system at the bottom of the LCZ which requires a circulating heat transfer fluid in a closed cycle (Lablanc et al., 2011). Additionally, heat recovery can be improved using the following methods: gravity assisted heat collection system (Tundee et al., 2010); bottom polystyrene insulation system (Ganguly et al., 2018); plastic cover for evaporation prevention (Ruskowitz et al., 2014); and fiber-optic sensors for NCZ erosion detection (Sarabia et al., 2018).

Ormat Turbines Ltd. (1981) numerically modeled the energy balance for a hypothetical pond with 1.0 km<sup>2</sup> surface area and 3.5% salt concentration (typical value for continental shelf seawater). The modeling indicated that part of the incoming solar insolation (20%) penetrates to the NCZ while 80% is reflected back to the atmosphere. Upon further penetration to the LCZ, minor amounts of solar energy are lost to the atmosphere (4%) and the ground (2%). Despite a low thermal efficiency (14%) of the pond, the entrapped thermal energy could warm up the LCZ to 65 °C under sunny climates. Similar successful industrial applications have been reported from other parts of the globe. For example, reaching up to 90 °C in a flotation cell using an annual solar insolation of 1600 kWh/m<sup>2</sup> in Granada, Spain (Alcaraz et al., 2018) and achieving an average air temperature of 40 °C utilizing an annual solar insolation of 1500 kWh/m<sup>2</sup> in Victoria, Australia (Bawahab et al. 2019).

### 2.3. Climatic Scoping

Figure 2 provides the global distribution of SGSP projects.

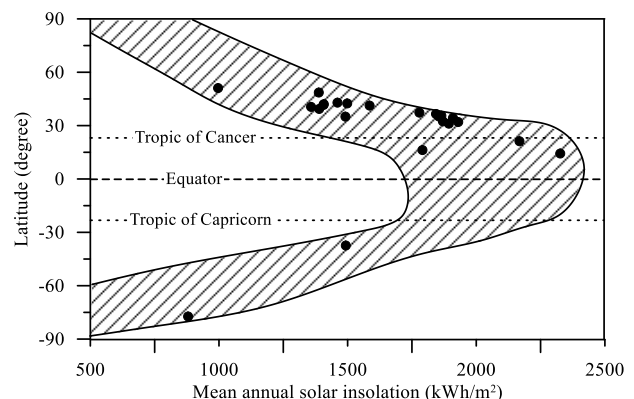


**Figure 2.** Global distribution of reported SGSP sites

Whereas such facilities can be developed across the globe, the majority of reported sites are located above the Tropic of Cancer ( $23.5^\circ$  N) at various elevations ranging from 6 m through 5000 m above mean sea level. In addition to latitude and altitude, the presence of adequate solar energy at a given site depends on local weather conditions. The influence of climatic factors on the efficiency of SGSP can be summarized as follows (Alenezi, 2012; Liu et al., 2015): (i) dilution of salts due to snowmelt improves solar penetration during spring-summer; (ii) turbidity due to rainfall and/or wind during summer-fall reduces solar penetration during summer; and (iii) snow cover offsets the low ambient air temperature during fall-winter.

Figure 3 plots the variation of mean annual solar insolation with respect to latitude such that the range is derived from the longitude. The data were obtained from the National Aeronautics and Space Administration of the United States of America (NASA Langley Research Center, 2018). The figure indicates two opposite trends, namely; an increase in solar insolation from the North Pole up to the Equator and a decrease from the Equator to the South Pole. The factors affecting the relatively larger range in solar insolation around equatorial regions are unknown. As expected, the reported SGSP sites were found to be within the range of variability. The actual value of solar insolation at a site depends on one or more of the following factors: (i) seasonal and daily weather variations; (ii) particulate matter and

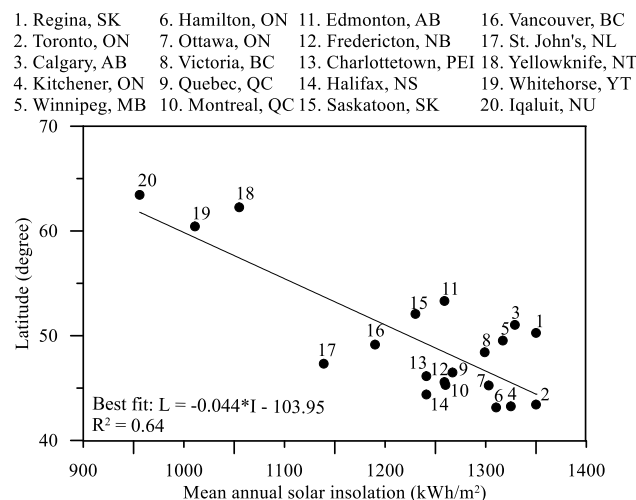
greenhouse gases in the atmosphere; and (iii) topographic features and elevation above mean sea level.



**Figure 3.** Global variation of solar insolation along with reported SGSP sites

Figure 4 gives the mean annual solar insolation in Canadian cities. The annual insolation ranges from  $956 \text{ kWh/m}^2$  in Iqaluit (Nunavut) to  $1350 \text{ kWh/m}^2$  in Regina (Saskatchewan). Cities in the Prairies (Regina, Calgary, and Winnipeg) generally rank higher and the annual insolation values in various locations cor-

relate with the latitude ( $R^2 = 0.64$ ). As mentioned earlier, latitude is not the only factor determining the annual insolation amount because locations of similar latitude are affected by seasonal weather and the site elevation (Nie et al., 2011). Nonetheless, French et al. (1985) concluded that SGSP is suitable for North American climate and that such facilities continuously produce heat required for domestic use in Ohio and industrial application in New Mexico.



**Figure 4.** Mean annual solar insolation in Canadian cities

### 3. Assessment of Criteria for SGSP Potential

#### 3.1. Salinity Based Criteria

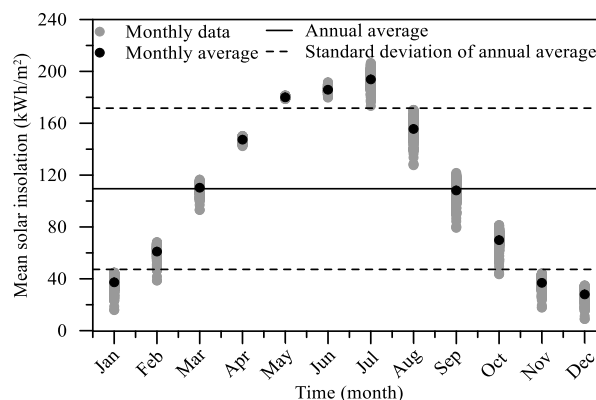
Saskatchewan hosts 535 natural saline water lakes (up to 10 km<sup>2</sup> and 5 m depth), which can be classified as follows: hypo-saline (3 ~ 20 g/L concentration); meso-saline (20 ~ 50 g/L concentration); and hyper-saline (> 50 g/L concentration). Normally, moderate water salinity ponds are dominated by Ca<sup>2+</sup>, Mg<sup>2+</sup>, and HCO<sub>3</sub><sup>-</sup> and higher water salinity ponds possess abundant Na<sup>+</sup> and Cl<sup>-</sup> (Hammer, 1986). These lakes were formed as a result of a deep collapse due to dissolution of Devonian evaporites (1000 m below surface) during the deglaciation period. High hydrostatic pressure exerted by excessive ground water recharge from melting glaciers burst the Tertiary and Quaternary sediments and fractures were developed. Transportation of saline water from below the Cretaceous aquifer was facilitated through these discontinuities in the bedrocks and formed saline lakes. Such conditions are prevalent across Central and Southern Saskatchewan (Christiansen, 1971). The total dissolved solids (TDS) for saline lakes ranges from 25 g/L to 250 g/L and these numbers are respectively equivalent to salt concentrations of 2.5 to 25% by mass (Bowman and Sachs, 2008).

Man-made saline water bodies (potash tailings ponds) result from wet mineral processing operations across Saskatchewan. According to Holter (1969), the above-mentioned Middle Devonian evaporites comprises of interbedded halite (sodium chloride, NaCl) and sylvite (potassium chloride, KCl).

The sylvite is extracted and the residual NaCl-rich slimes are disposed of in designated containment areas (1 ~ 4 km<sup>2</sup>) at high slopes (30 ~ 40°) near the discharge points that gradually diminishes to form a brine pond at the toe of the hill (Tallin et al., 1990). The TDS for typical potash tailings storage facilities is 360 g/L corresponding to 36% salt concentration by mass (Landine, 1993).

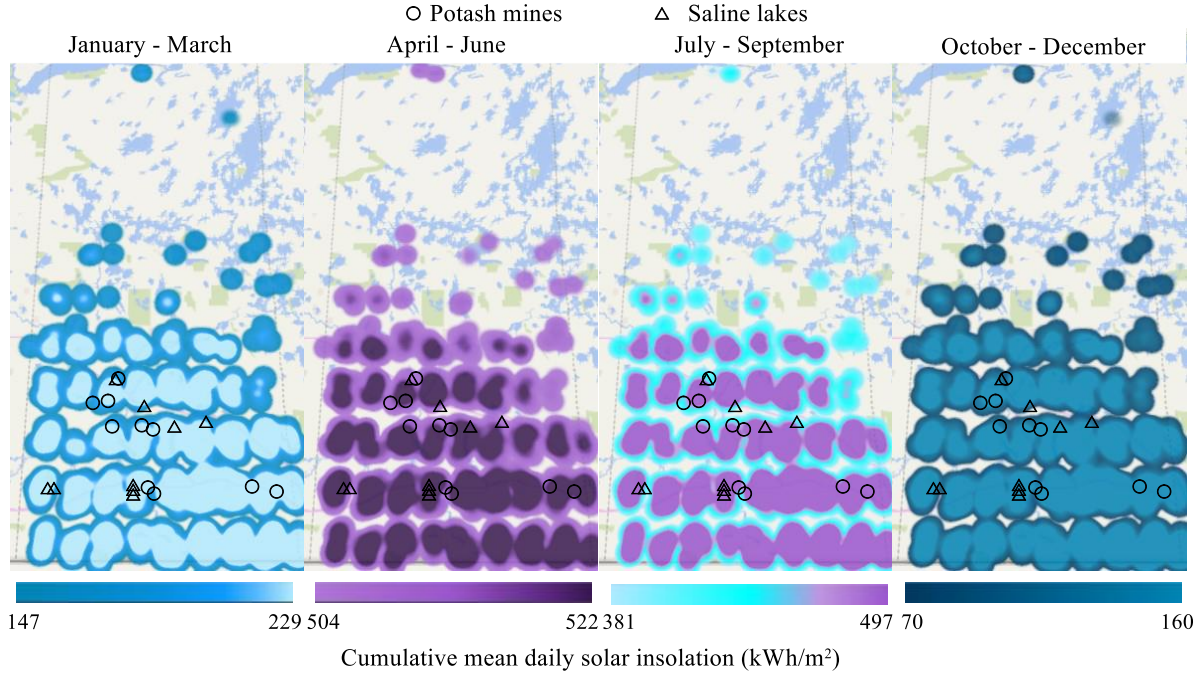
#### 3.2. Climate Based Criteria

Figure 5 gives the monthly variabilities of average solar insolation in Saskatchewan. The monthly solar insolation periodically oscillates with an amplitude of  $\pm 80$  kWh/m<sup>2</sup> (standard deviation) from the mean value of 110 kWh/m<sup>2</sup> with extreme values ranging from as high as 190 kWh/m<sup>2</sup> in July to as low as 30 kWh/m<sup>2</sup> in December. This is due to seasonal changes in the instantaneous measurement of solar power per unit area (that is, irradiance is maximum in summer and minimum in winter for the northern hemisphere of the globe). Furthermore, the insolation variability within the summer months is negligible across Saskatchewan because the higher day length in the north is compensated by a low irradiance and vice versa. These results correlate well with the photovoltaic potential (kWh/kW) map calculated on the basis of solar insolation values (Pelland et al., 2006). This means that the entire province is suitable for a stable solar energy harvesting during summer.

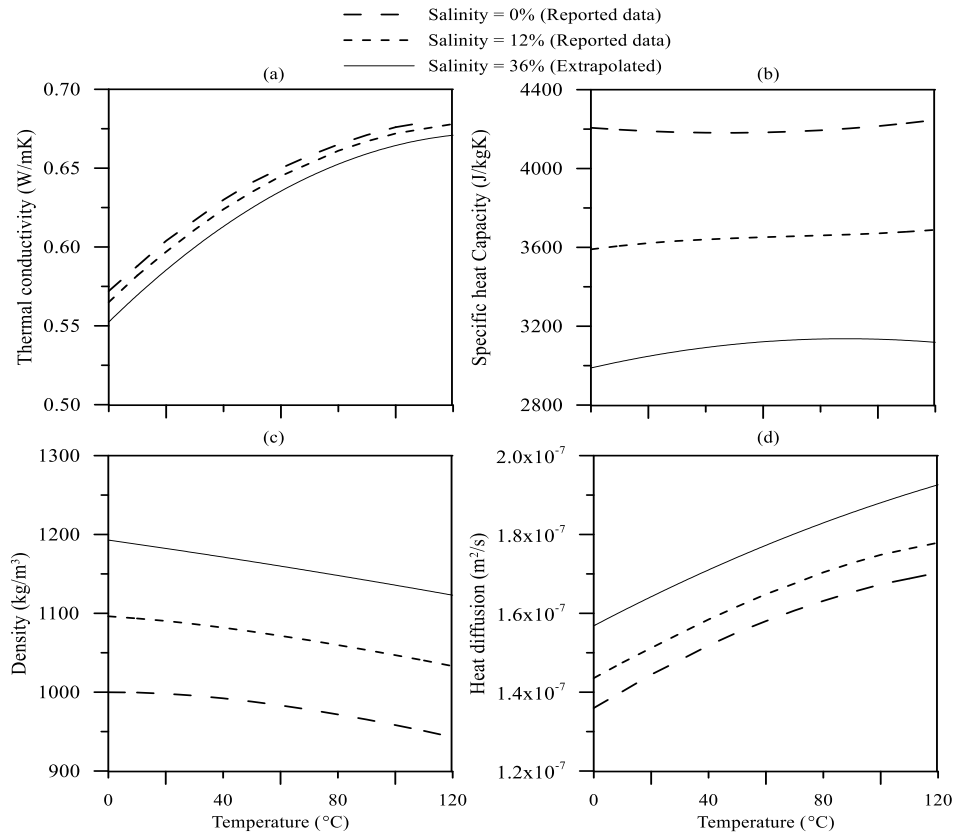


**Figure 5.** Monthly variation of solar insolation in Saskatchewan

Figure 6 illustrates the solar insolation map superimposed with saline water systems (10 potash mine sites and 10 saline water lakes) in Saskatchewan. These sites are located in southern Saskatchewan between the latitude 50°25' and 52°70'. The seasonal variation (every three months period) of solar insolation throughout the year is color coded. As mentioned above, the composition of saline water bodies indicated abundant NaCl and minor amounts of KCl. Finally, the investigated potash tailings containment facilities with 36% salinity and at least two saline lakes with 25% salinity (Chaplin and Ingebrigt) are suitable SGSP candidates receiving 1300 kWh/m<sup>2</sup> of solar insolation annually. The latter data for these sites falls within the range for SGSP selection, as described earlier in Figure 3 (1100 and 1400 kWh/m<sup>2</sup>).



**Figure 6.** Seasonal solar insolation maps of Saskatchewan along with saline water bodies (Data from National Resources Canada, 2018)



**Figure 7.** Variation of thermophysical properties with temperature for water with varying salinity



## 4. Conceptual Modeling

### 4.1. Factors Affecting Heat Transfer in SGSP

Figure 7 gives the variation of thermophysical properties of saline waters with respect to temperature from 0° to 120°: (a) thermal conductivity ( $k$ , W/m K); (b) specific heat capacity ( $C_p$ , J/kg K), (c) density ( $\rho$ , kg/m<sup>3</sup>); and (d) coefficient of heat diffusion ( $\alpha$ , m<sup>2</sup>/s). The reported data for 0% to 12% salinity (Mostafa et al., 2010; Nayar et al., 2016) were used to extrapolate the thermophysical properties for 36% water salinity (corresponding to concentration of potash tailings). The figure indicates that thermal conductivity increases with temperature raise but decreases with an increase in salinity; the opposite is true for density. Similarly, specific heat capacity slightly increases with temperature and is inversely correlated with salinity. The coefficient of heat diffusion was calculated according to the following expression (Bird et al., 2006):

$$\alpha = k / (\rho C_p) \quad (1)$$

The above equation means that the coefficient of heat diffusion is directly proportional to thermal conductivity and inversely proportional to specific heat capacity and density. The corresponding polynomial fits for the above-mentioned properties depend on temperature ( $T$ , °C), as given below:

$$k = -7 \times 10^{-6} T^2 + 0.002T + 0.6 \quad (2)$$

$$C_p = -320 \times 10^{-6} T^2 + 5.211T + 2480 \quad (3)$$

$$\rho = -100 \times 10^{-6} T^2 - 0.596T + 1190 \quad (4)$$

When water is heated by solar radiation, the energy is transferred to increase the rates of rotational, vibrational, and translational motions. In freshwater, heat is conducted through water molecules forming polymer-like chains by connecting up to eight molecules. Some of these chains are disrupted in saline waters due to the presence of ions such as Na<sup>+</sup> and Cl<sup>-</sup> thereby forming a mixture of linked water molecules and free water molecules. This is why thermal conductivity (ability to transfer heat) is maximum for freshwater through the chains and decreases with increasing salt concentration (Talley et al., 2011). In contrast, the specific heat capacity (amount of heat needed to raise the temperature of 1 kg mass by 1 °C) decreases with increasing salt concentration because the relative number of free water molecules in a concentrated solution is higher (more disruptions of the chains) than that in freshwater. This means that the presence of hydrogen bonds creating the water molecule chains are reduced and less energy is required to heat salt water (Brini et al., 2017). Furthermore, the density of salt water is affected by the molecular weight of a solute which increases with an increase in brine concentration (Dincer and Rosen, 2011).

Figure 7 confirms previous observations (Wei, 2015) for the investigated ranges, that is, salinity dependent fluctuations in specific heat capacity (3000 ~ 4200 J/kg K) and density (1000 ~ 1200 kg/m<sup>3</sup>) are higher than those in the thermal con-

ductivity (0.55 ~ 0.675 W/mK). Consequently, the coefficient of heat diffusion increases with an increase in salt concentration and temperature.

### 4.2. Heat Diffusion Modeling for SGSP

Using  $t$  for time (s), and  $y$  for pond depth (m), a heat diffusion model was developed for SGSP in the LCZ (where the heat is mostly stored, Figure 1) based on the following equation (Bird et al., 2006):

$$\frac{\partial T}{\partial t} = \alpha \frac{\partial^2 T}{\partial y^2} \quad (5)$$

The quasi-one dimensional model (length in x-direction = 1/10 length in y-direction) used a 1 m deep LCZ along with transient heat diffusion coefficients at selected time steps of 1, 5, 10, 15, 20, 25, and 30 days. The Dirichlet boundary condition (corresponding to 36% water salinity and receiving 180 kWh/m<sup>2</sup>) was applied at the top and the Neumann boundary condition ( $\partial T / \partial t = 0$  because only 2% heat is lost) was applied at the bottom. The initial condition was set to 20 °C corresponding to the average ambient air temperature.

A partial differential equation solver (FlexPDE) was used for simulating heat diffusion. Based on the finite element method, the solver automatically generated an initial triangular mesh for the prescribed geometry. The governing equation along with the thermophysical property functions (given in Figure 7) were used as model inputs. The compiler carried out spatial and temporal refinement of the initial mesh through automatic mesh refinement to reduce the error within the tolerance limit for the selected units. The model output was in the form of temperature (°C) versus pond depth (m) for selected time intervals over one month period.

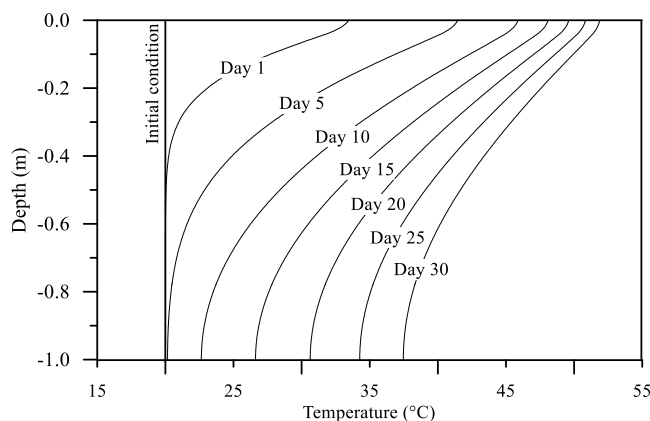
Table 1 summarizes the specific data of model development using mesh testing. The default setting of the solver pertained to an initial mesh at the densest possible configuration. The optimum initial mesh density was evaluated for 10%, 50%, and 100% of the default setting. The automatic mesh refinement function achieved convergence (with marginal error) such that the computing time remained constant (10 seconds) for all cases. The 50% of default setting was found to be the optimum and was used as the initial mesh density for subsequent analysis.

**Table 1.** Summary of Mesh Tests

Initial mesh density	Nodes	Cells	Cycles	Error ( $\times 10^{-7}$ )
10% of Default	71	28	93	10.7
50% of Default	74	29	101	9.2
100% of Default	97	34	97	9.4

Figure 8 presents temperature profiles for a 1 m thick NCZ in a typical SGSP for potash tailings containment facility. The temperature was found to decrease from a high value at the surface (solar radiation coming from above) to a lower value at the bottom following a curvilinear path that approach the bound-

aries at right angles. This means that the model captures the cumulative effect of temperature increase that, in turn, affects each of the thermophysical property (Figure 7). When the family of curves is considered as a whole, two sets of temperature increases are observed at the top: a rapid increase in the first 10 days (from 20 to 46 °C) and a low increase in the last 20 days (from 46 to 52 °C). This is attributed to the diminishing gradient between the surface and the adjacent lower layer (that absorbs the temperature from above) and the effect is carried forward to the next time step. In contrast, the temperature increase was found to be fairly constant ( $3.5 \pm 0.6$  °C for every 10 day period) at the pond bottom owing to the applied negligible energy loss at that boundary. Finally, the family of curves tend to approach the surface temperature over time even without convection thereby confirming model applicability to SGSP albeit the absolute values of temperature may vary depending on actual field conditions.



**Figure 8.** Results of quasi one-dimensional heat diffusion model for SGSP

The conceptual model presented in this paper is at a preliminary stage of development. The following recommendations should be considered for an improved numerical prediction of SGSP: (i) consider convection currents due to heat diffusion within the LCZ; (ii) replicate complex interactions within UCZ, NCZ, and LCZ during heat diffusion; (iii) refine boundary conditions using actual weather data including precipitation, air temperature, wind speed, relative humidity, and daily sunlight duration and amount; (iv) calibrate and verify the modeling results with bench-scale physical models tested under controlled environments; and (v) validate the model by conducting pilot-scale SGSP field testing. To develop a comprehensive understanding of SGSP for Saskatchewan, risk assessments is recommended for aquatic life, ground water, surface flooding, air quality, algal growth, and convective currents.

## 5. Summary and Conclusion

Knowledge of saline gradient solar ponds is critical as a sustainable (cost-effective, environmentally friendly, and socially viable) source of thermal energy. This paper evaluated the feasibility of SGSP as an alternative energy source for

Saskatchewan, Canada. The main achievements of this research were the following: (i) global appraisal of SGSP from theoretical and practical perspectives; (ii) assessment of salinity and climatic criteria for SGSP potential; (iii) clear understanding of heat transfer mechanisms as influenced by thermophysical properties; and (iv) numerical modeling to simulate transient heat diffusion in SGSP. Globally, industrial applications such as mineral production and desalination plants, have SGSP potential provided local climatic conditions are conducive. The main conclusions of the study are given below:

1. Saskatchewan is ideal for SGSP because of a relatively high solar insolation (1100 to 1400 kWh/m<sup>2</sup>). The solar radiation in such systems is captured at the bottom under a vertical salt concentration profile. Based on spatio-temporal correlations, ten potash tailings sites (360 or 36% salt concentration) and two saline water lakes (250 g/L or 25% salt concentration) are identified as potentially suitable SGSP candidates.
2. Thermal conductivity was found to increase with temperature raise but decreased with an increase in water salinity (0.55 ~ 0.675 W/m K), the opposite trend was found to be true for density (1000 to 1200 kg/m<sup>3</sup>). Likewise, specific heat capacity was found to slightly increase with temperature and inversely correlated with water salinity (3000 ~ 4200 J/kg K).
3. The heat diffusion model adequately simulated the temperature distribution profile for a typical SGSP in a potash tailings containment facility. For the investigated month of July (highest solar insolation), the temperatures increased from an initial value of 20 to 52 °C at top to 37 °C at bottom. A comprehensive risk assessment of this method is required to protect air, water, soil, and biota at specific sites.

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